

AUDIO-FREQUENCY POWER AMPLIFIER AND MODULATOR

 Class-AB₁.

MAXIMUM RATINGS

D-C PLATE VOLTAGE	-	-	-	-	-	3000 MAX. VOLTS
D-C SCREEN VOLTAGE	-	-	-	-	-	600 MAX. VOLTS
MAX-SIGNAL D-C PLATE CURRENT, PER TUBE	-	-	-	-	-	225 MAX. MA
PLATE DISSIPATION, PER TUBE	-	-	-	-	-	125 MAX. WATTS
SCREEN DISSIPATION, PER TUBE	-	-	-	-	-	20 MAX. WATTS

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D-C PLATE VOLTAGE	-	-	-	-	-	3000 MAX. VOLTS
D-C SCREEN VOLTAGE	-	-	-	-	-	400 MAX. VOLTS
MAX-SIGNAL D-C PLATE CURRENT, PER TUBE	-	-	-	-	-	225 MAX. MA
PLATE DISSIPATION, PER TUBE	-	-	-	-	-	125 MAX. WATTS
SCREEN DISSIPATION, PER TUBE	-	-	-	-	-	20 MAX. WATTS

TYPICAL OPERATION (Sinusoidal wave, two tubes unless otherwise specified)

D-C Plate Voltage	-	-	-	1500	2000	2500	volts
D-C Screen Voltage	-	-	-	600	600	600	volts
D-C Grid Voltage ²	-	-	-	-90	-94	-96	volts
Zero-Signal D-C Plate Current	-	-	-	60	50	50	ma
Max-Signal D-C Plate Current	-	-	-	222	240	232	ma
Zero-Signal D-C Screen Current	-	-	-	-1.0	-0.5	-0.3	ma
Max-Signal D-C Screen Current	-	-	-	17	6.4	8.5	ma
Effective Load, Plate-to-Plate	-	-	-	10,200	13,400	20,300	ohms
Peak, A-F Grid Input Voltage (per tube)	-	-	-	90	94	96	volts
Driving Power	-	-	-	0	0	0	watt
Max-Signal Plate Dissipation (per tube)	-	-	-	87.5	125	125	watts
Max-Signal Plate Power Output	-	-	-	158	230	330	watts
Total Harmonic Distortion	-	-	-	5	2	2.6	per cent

TYPICAL OPERATION (Sinusoidal wave, two tubes unless otherwise specified)

D-C Plate Voltage	-	-	-	1500	2000	2500	volts
D-C Screen Voltage	-	-	-	350	350	350	volts
D-C Grid Voltage	-	-	-	-41	-45	-43	volts
Zero-Signal D-C Plate Current	-	-	-	87	72	93	ma
Max-Signal D-C Plate Current	-	-	-	400	300	260	ma
Zero-Signal D-C Screen Current	-	-	-	0	0	0	ma
Max-Signal D-C Screen Current	-	-	-	34	5	6	ma
Effective Load, Plate-to-Plate	-	-	-	7200	13,600	22,200	ohms
Peak A-F Grid Input Voltage (per tube)	-	-	-	141	105	89	volts
Max-Signal Avg. Driving Power (approx.)	-	-	-	2.5	1.4	1	watts
Max-Signal Peak Driving Power	-	-	-	5.2	3.1	2.4	watts
Max-Signal Plate Dissipation (per tube)	-	-	-	125	125	122	watts
Max-Signal Plate Power Output	-	-	-	350	350	400	watts
Total Harmonic Distortion	-	-	-	2.5	1	2.2	per cent

¹ The effective grid circuit resistance for each tube must not exceed 250,000 ohms.

² Driving power increases above 70 Mc. See page 4.

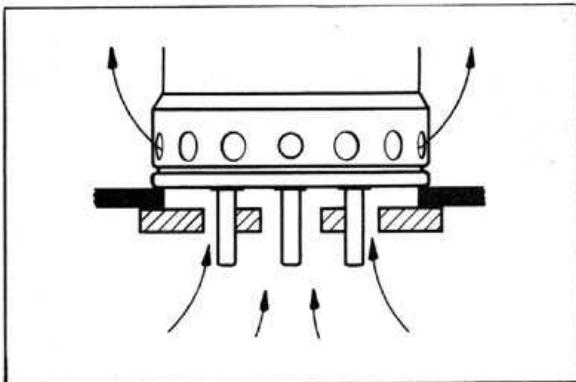
IF IT IS DESIRED TO OPERATE THIS TUBE UNDER CONDITIONS WIDELY DIFFERENT FROM THOSE GIVEN UNDER "TYPICAL OPERATION," POSSIBLY EXCEEDING THE MAXIMUM RATINGS GIVEN FOR CW SERVICE, WRITE EITEL-MCCULLOUGH, INC., FOR INFORMATION AND RECOMMENDATIONS.

APPLICATION

MECHANICAL

► **Mounting**—The 4-125A must be mounted vertically, base down or base up. The socket must be constructed so as to allow an unimpeded flow of air through the holes in the base of the tube and must also provide clearance for the glass tip-off which extends from the center of the base. The tube should be mounted above the chassis deck to allow free circulation of air in the manner shown in the mounting diagram below. The above requirements are met by the E. F. Johnson Co. socket No. 122-275, the National Co. socket No. HX-100, or a similar socket.

A flexible connecting strap should be provided between the HR-6 Heat Dissipating Plate Connector on the plate terminal and the external circuit. The tube must be protected from severe vibration and shock.



4-125A mounting providing base cooling, shielding and isolation of output and input compartments.

Cooling—Adequate cooling must be provided for the seals and envelope of the 4-125A. In continuous-service applications, the temperature of the plate seal, as measured on the top of the plate cap, should not exceed 170° C. A relatively slow movement of air past the tube is sufficient to prevent seal temperatures in excess of maximum at frequencies below 30 Mc. At frequencies above 30 Mc., radio-frequency losses in the leads and envelope contribute to seal and envelope heating, and special attention should be given to cooling. A small fan or centrifugal blower directed toward the upper portion of the envelope will usually provide sufficient circulation for cooling at frequencies above 30 Mc., however.

► Indicates change from sheet dated 3-15-50

In intermittent-service applications where the "on" time does not exceed a total of five minutes in any ten-minute period, plate seal temperatures as high as 220° C. are permissible. When the ambient temperature does not exceed 30° C. it will not ordinarily be necessary to provide forced cooling to hold the temperature below this maximum at frequencies below 30 Mc., provided that a heat-dissipating plate connector is used, and the tube is so located that normal circulation of air past the envelope is not impeded.

Provision must be made for circulation of air through the base of the tube. Where shielding or socket design makes it impossible to allow free circulation of air through the base, it will be necessary to apply forced-air cooling to the stem structure. An air flow of two cubic feet per minute through the base will be sufficient for stem cooling.

ELECTRICAL

Filament Voltage—For maximum tube life the filament voltage, as measured directly at the filament pins, should be the rated value of 5.0 volts. Unavoidable variations in filament voltage must be kept within the range from 4.75 to 5.25 volts.

Bias Voltage—D-c bias voltage for the 4-125A should not exceed 500 volts. If grid-leak bias is used, suitable protective means must be provided to prevent excessive plate or screen dissipation in the event of loss of excitation.

Screen Voltage—The d-c screen voltage for the 4-125A should not exceed 400 volts, except for class-AB₁ audio operation.

Plate Voltage—The plate-supply voltage for the 4-125A should not exceed 3000 volts for frequencies below 120 Mc. The maximum permissible plate voltage is less than 3000 volts above 120 Mc., as shown by the graph on page 4.

Grid Dissipation—Grid dissipation for the 4-125A should not be allowed to exceed five watts. Grid dissipation may be calculated from the following expression:

$$P_g = e_{cmpl}$$

where P_g = Grid dissipation,
 e_{cmpl} = Peak positive grid voltage, and

$$I_g = D-c \text{ grid current.}$$

e_{cmpl} may be measured by means of a suitable peak voltmeter connected between filament and grid⁴.

Screen Dissipation—The power dissipated by the screen of the 4-125A must not exceed 20 watts. Screen dissipation is likely to rise to excessive values when the plate voltage, bias voltage or plate load are removed with filament and screen voltages applied. Suitable protective means must be provided to limit screen dissipation to 20 watts in the event of circuit failure.

⁴ For suitable peak v.t.v.m. circuits see, for instance, "Vacuum Tube Ratings," Eimac News, January, 1945. This article is available in reprint form on request.

Plate Dissipation—Under normal operating conditions, the plate dissipation of the 4-125A should not be allowed to exceed 125 watts in unmodulated applications.

In high-level-modulated amplifier applications, the maximum allowable carrier-condition plate dissipation is 85 watts. The plate dissipation will rise to 125 watts under 100% sinusoidal modulation.

Plate dissipation in excess of the maximum rating is permissible for short periods of time, such as during tuning procedures.

OPERATION

Class-C Telegraphy or FM Telephony—The 4-125A may be operated as a class-C telegraph or FM telephone amplifier without neutralization up to about 30 Mc. if reasonable precautions are taken to prevent coupling between input and output circuits external to the tube. A grounded metallic plate on which the socket may be mounted as shown in the mounting diagram on page two provides an effective isolating shield between grid and plate circuits. In single-ended circuits, plate, grid, filament and screen by-pass capacitors should be returned through the shortest possible leads to a common chassis point. In push-pull applications the filament and screen terminals of each tube should be by-passed to a common chassis point by the shortest possible leads, and short, heavy leads should be used to interconnect the screens and filaments of the two tubes. Care should be taken to prevent leakage of radio-frequency energy to leads entering the amplifier, to prevent grid-plate coupling between these leads external to the amplifier.

Where shielding is adequate, the feed-back at frequencies above 100 Mc. is due principally to screen-lead-inductance effects, and it becomes necessary to introduce in-phase voltage from the plate circuit into the grid circuit. This can be done by adding capacitance between plate and grid external to the tube. Ordinarily, a small metal tab approximately $\frac{3}{4}$ -inch square connected to the grid terminal and located adjacent to the envelope opposite the plate will suffice for neutralization. Means should be provided for adjusting the spacing between the neutralizing capacitor plate and the envelope, but care must be taken to prevent the neutralizing plate from touching the envelope. An alternative neutralization scheme is illustrated in the diagram below. In this circuit feed-back is eliminated by series-tuning the screen to ground with a small capacitor. The socket screen terminals should be strapped together, as shown on the diagram, by the shortest possible lead, and the leads from the screen terminal to the capacitor, C, and from the capacitor to ground should be made as short as possible. All connections to the screen terminals should be made to the center of the strap between the terminals, in order to equalize the current in the two screen leads and prevent overheating one of them. The value for C given under the diagram presupposes the use of the shortest possible leads.

At frequencies below 100 Mc. ordinary neutralization systems may be used. With reasonably effective shielding, however, neutralization should not be required below about 30 Mc.

The driving power and power output under typical operating conditions, with maximum output and plate voltage, are shown on page 4. The power output shown is the actual plate power delivered by the tube; the power delivered to the load will depend upon the efficiency of the plate tank and output coupling system. The driving power is likewise the driving power required by the tube (includes bias loss). The driver output power should exceed the driving power requirement by a sufficient margin to allow for coupling-circuit losses. These losses will not ordinarily amount to more than 30 or 40 per cent of the driving power, except at frequencies above 150 Mc. The use of silver-plated linear tank-circuit elements is recommended at frequencies above 100 Mc.

Conventional capacitance-shortened quarter-wave linear grid tank circuits

having a calculated Z_0 of 160 ohms or less may be used with the 4-125A up to 175 Mc. Above 175 Mc. linear grid tank circuits employing a "capacitor"-type shorting bar, as illustrated in the diagram below, may be used. The capacitor, C₁, may consist of two silver-plated brass plates one inch square with a piece of .010-inch mica or polystyrene as insulation.

Class-C AM Telephony—The r-f circuit considerations discussed above under Class-C Telegraphy or FM Telephony also apply to amplitude-modulated operation of the 4-125A. When the 4-125A is used as a class-C high-level-modulated amplifier, modulation should be applied to both plate and screen. Modulation voltage for the screen may be obtained from a separate winding on the modulation transformer, by supplying the screen voltage via a series dropping resistor from the unmodulated plate supply, or by the use of an audio-frequency reactor in the positive screen-supply lead. When screen modulation is obtained by either the series-resistor or the audio-reactor method, the audio-frequency variations in screen current which result from variations in plate voltage as the plate is modulated automatically give the required screen modulation. Where a reactor is used, it should have a rated inductance of not less than 10 henries divided by the number of tubes in the modulated amplifier and a maximum current rating of two or three times the operating d-c screen current. To prevent phase shift between the screen and plate modulation voltages at high audio frequencies, the screen by-pass capacitor should be no larger than necessary for adequate r-f by-passing. Where screen voltage is obtained from a separate winding on the modulation transformer, the screen winding should be designed to deliver the peak screen modulation voltage given in the typical operating data on page 1.

For high-level modulated service, the use of partial grid-leak bias is recommended. Any by-pass capacitors placed across the grid-leak resistance should have a reactance at the highest modulation frequency equal to at least twice the grid-leak resistance.

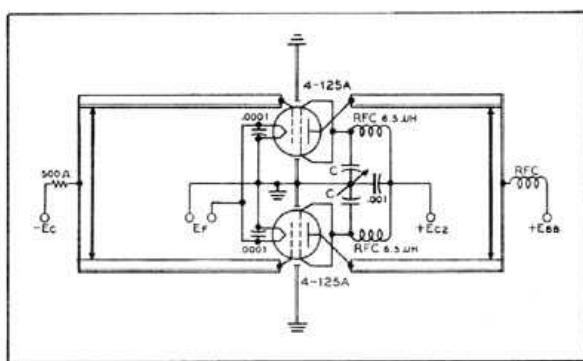
Class-AB₁ and Class-AB₂ Audio—Two 4-125A's may be used in a push-pull circuit to give relatively high audio output power at low distortion. Maximum ratings and typical operating conditions for class-AB₁ and class-AB₂ audio operation are given in the tabulated data.

When type 4-125A tubes are used as class-AB₁ or class-AB₂ audio amplifiers at 1500 plate volts, under the conditions given under "Typical Operation," the screen voltage must be obtained from a source having reasonably good regulation, to prevent variations in screen voltage from zero-signal to maximum-signal conditions. The use of voltage regulator tubes in a standard circuit will provide adequate regulation. The variation in screen current of plate voltages of 2000 and above is low enough so that any screen power supply having a normal order of regulation will serve. The driver plate supply makes a convenient source of screen voltage under these conditions.

Grid bias voltage for class-AB₂ service may be obtained from batteries or from a small fixed-bias supply. When a bias supply is used, the d-c resistance of the bias source should not exceed 250 ohms. Under class-AB₁ conditions the effective grid-circuit resistance for each tube should not exceed 250,000 ohms.

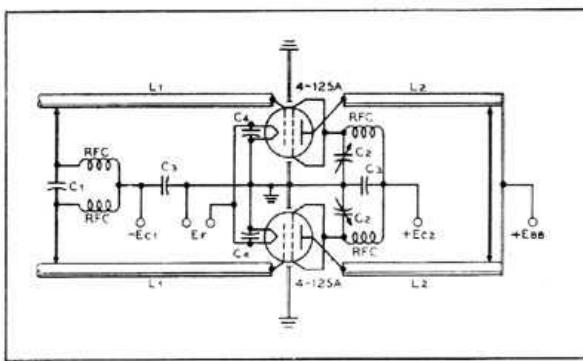
The peak driving power figures given in the class-AB₂ tabulated data are included to make possible an accurate determination of the required driver output power. The driving amplifier must be capable of supplying the peak driving power without distortion. The driver stage should, therefore, be capable of providing an undistorted average output equal to half the peak driving power requirement. A small amount of additional driver output should be provided to allow for losses in the coupling transformer.

The power output figures given in the tabulated data refer to the total power output from the amplifier tubes. The useful power output will be from 5 to 15 per cent less than the figures shown, due to losses in the output transformer.



Screen-tuning neutralization circuit for use above 100 Mc.
C is a small split-stator capacitor.

$$C_{1\mu\text{fd}} = \frac{640,000}{f^2 \text{ (Mc.)}}, \text{ approx.}$$



Typical circuit arrangement useful for frequencies above.

175 Mc.

C₁—See above.

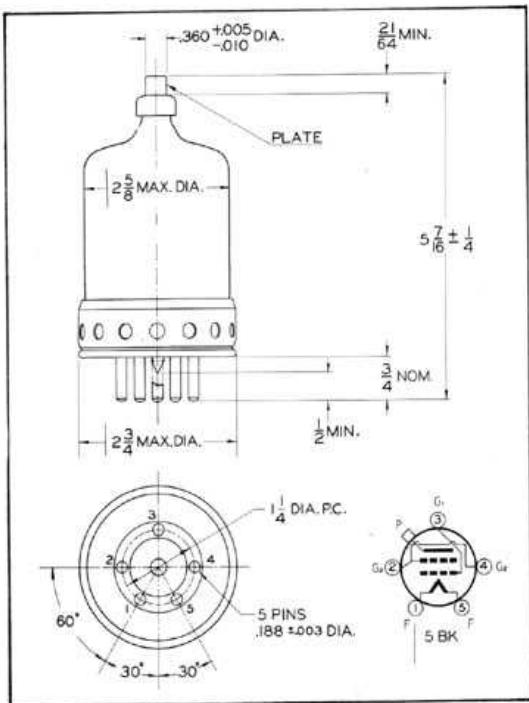
C₂—Neutralizing capacitor.

C₃—.001 μ fd.

C₄—100 μ fd.

L₁— $\frac{3}{8}$ " dia. copper spaced,
1" center-to-center, 6" long.

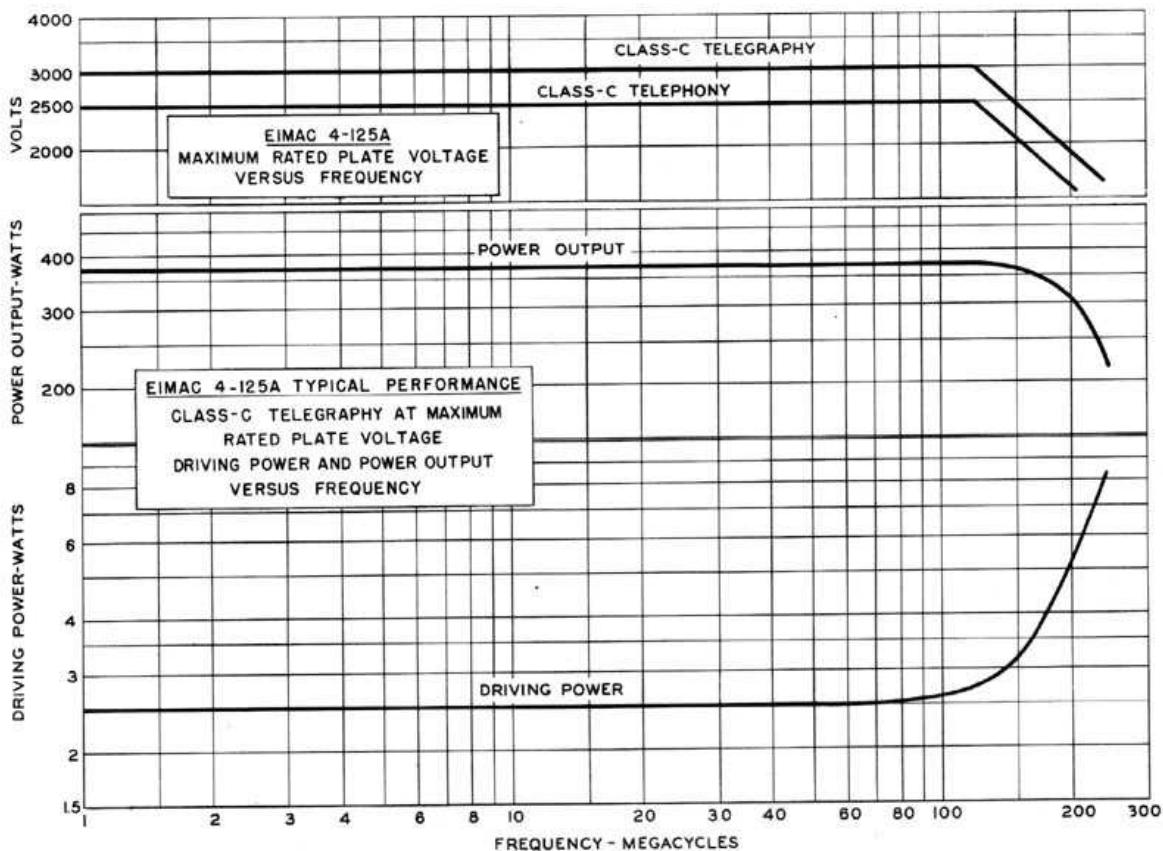
L₂— $\frac{7}{8}$ " dia. brass, silver plated,
spaced 1 $\frac{1}{2}$ " center-to-center,
14" long.

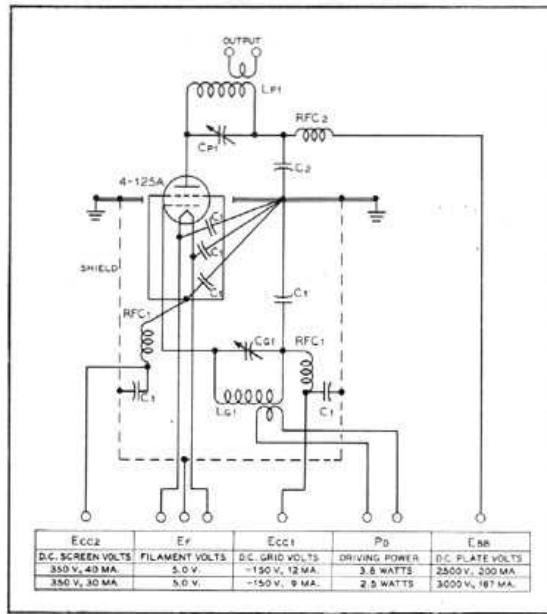


COMPONENTS FOR TYPICAL CIRCUITS

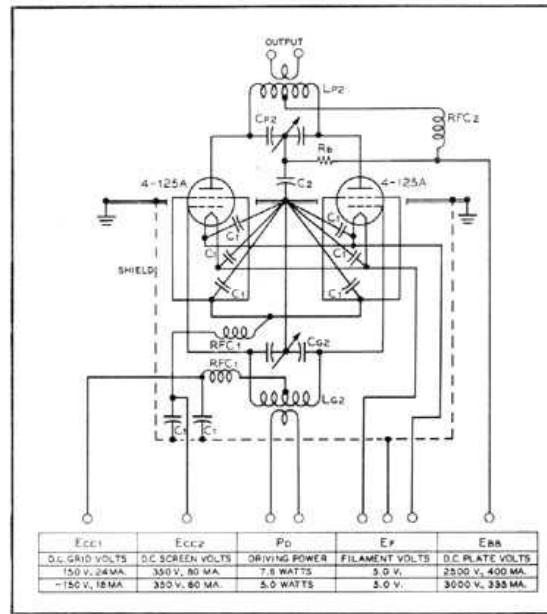
(Diagrams, Page 5)

L_{p1} - C_{p1} —Tank circuit appropriate for operating frequency; $Q = 12$.
 Capacitor plate spacing = .200".
 L_{p2} - C_{p2} —Tank circuit appropriate for operating frequency; $Q = 12$.
 Capacitor plate spacing = .200".
 L_{p3} - C_{p3} —Tank circuit appropriate for operating frequency; $Q = 12$.
 Capacitor plate spacing = .375".
 L_{p4} - C_{p4} —Tank circuit appropriate for operating frequency; $Q = 12$.
 Capacitor plate spacing = .375".
 L_{g1} - C_{g1} —Tuned circuit appropriate for operating frequency.
 L_{g2} - C_{g2} —Tuned circuit appropriate for operating frequency.
 C1—.002- μ fd., 500-v. mica
 C2—.002- μ fd., 5000-v. mica
 C3—.001- μ fd., 2500-v. mica
 C4—16- μ fd., 450-v. electrolytic
 C5—10- μ fd., 25-v. electrolytic
 R1—7000 ohms, 5 watts
 R2—70,000 ohms, 100 watts
 R3—3500 ohms, 5 watts
 R4—35,000 ohms, 200 watts
 R5—560 ohms, 1 watt
 R6—25,000 ohms, 2 watts
 R7—1500 ohms, 5 watts
 RFC1—2.5-mhy., 125-ma. r-f choke
 RFC2—1-mhy., 500-ma. r-f choke
 T1—10-watt driver transformer; ratio pri. to $1/2$ sec. approx. 2:1;
 T2—200-watt modulation transformer; ratio pri. to sec. approx. 1:1;
 pri. impedance = 16,200 ohms, sec. impedance = 16,500 ohms.
 T3—5-watt driver transformer; ratio pri. to $1/2$ sec. approx. 1:1:1.
 T4—400-watt modulation transformer; ratio pri. to sec. approx. 2.7:1;
 pri. impedance = 22,200 ohms, sec. impedance = 8300 ohms.

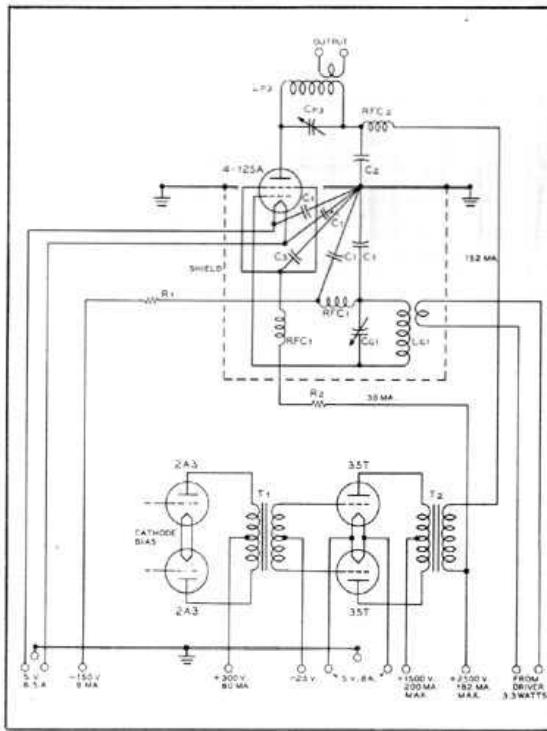




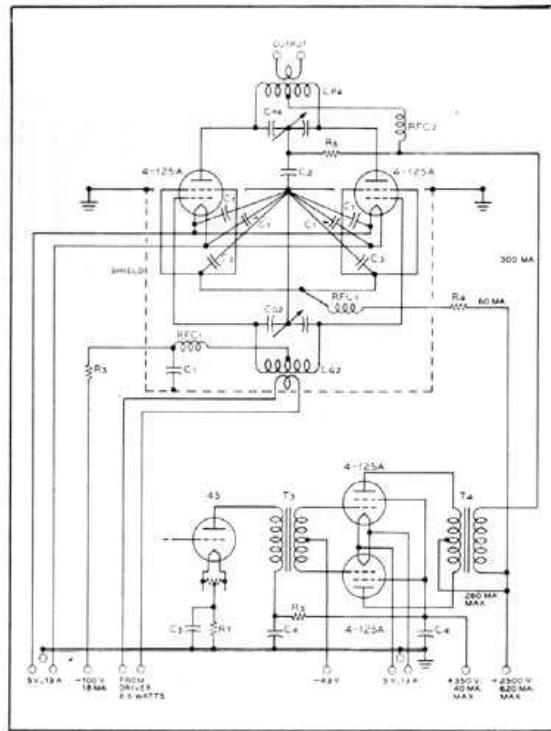
Typical radio-frequency power amplifier circuit, Class-C telegraphy, 500 watts input.



Typical radio-frequency power amplifier circuit, Class-C telegraphy, 1000 watts input.



Typical high-level-modulated r-f amplifier circuit, with modulator and driver stages, 380 watts plate input.



Typical high-level-modulated r-f amplifier circuit, with modulator and driver stages, 750 watts plate input.

SEE PRECEDING PAGE FOR LIST OF COMPONENTS

